

Inverted T-Slot Compact Microstrip Antennas for Multiband Operations

Ratnesh Kumari, Mithilesh Kumar

Abstract— In the days of modern communication, the compact size, low profile antenna with the directional capability is demanded for the wireless communication applications. To fulfill this requirement two new structures of antennas are designed. Two different geometries of microstrip antenna for triple band and Tetra band operation have been investigated in this paper with a new concept of T-slot in the radiating element of antenna and an E-slot in the ground plan of the antenna. For the wideband operation the partial ground with E-slot is used. The designed structure can be used for the multiband operation with the directional radiation pattern and the return loss of the antenna is below -10 dB. The resonant frequency band shown by the first structure is centered at the 3.4 GHz, 7.4 GHz and 10.6 GHz. One frequency band is increased by changing the ground parameter of the first structure thus second structure works at the four frequency bands which are centered at the 4.4 GHz, 5.3 GHz, 8.6 GHz and 11.2 GHz with improving results of the antenna.

These antennas, proposed and modified structure have small size of $22 \times 16 \times 1 \text{ mm}^3$ with the ground plane. For designing of these structure FR-4 substrate of thickness $h = 1 \text{ mm}$ with Dielectric constant = 4.05 and loss tangent of the antenna is 0.02 is used. CST microwave studio software is used for the simulation of the designed structures.

Index Terms—Compact antenna, microstrip feed line, multiband, resonance frequency, Inverted T-slot, E-slot.

1 INTRODUCTION

In these days the demand of multiband antennas are increasing rapidly in various communication services like:- (a) WiMAX (Worldwide Interoperability for Microwave Access) (b) WLAN (Wireless Local Area Network) (c) GSM (Global System for Mobile communications) (d) UMTS (Universal Mobile Telecommunications System) (e) DCS (Digital Communication Systems) and many other wireless applications. These wireless communication services require the broadband and multiband antennas in place of narrowband antennas for better performances [1].

So, the modern wireless communication devices want the single one antenna which can operate more than one frequency band. For multiband operation mainly ultra wideband antenna is designed. When antenna works for the good performance then the miniaturization is the main issue in these antennas. To minimize this issue in multiband antennas we use the planar printed monopole antennas due to its simple structure and low cost, these antennas also have the feature of ease of fabrication, wide bandwidth and Omni-directional radiation pattern [2],[3],[4],[5],[6],[7].

Bandwidth also a main parameter in the multiband antennas so there are so many techniques are used for increasing the bandwidth of these antennas. Some techniques use in the ground plan of the antenna like L-shaped notch in the lower corner is used in the truncated ground plane [8],[9] and in the middle of the ground an inverted T-shaped notch in the middle of the truncated ground plane is used for enhancing the bandwidth of the antenna [10].

Recently, the enhancement of the resonant frequency band also become popular parameter in the communication devices for this two slot are used in the ground plane and the bandwidth of antenna is also enhanced [11].

These antennas are not sufficient for filling the all requirement of the multiband operation so for increasing the band of the antenna a new technique used in this is a T-slot on the top of

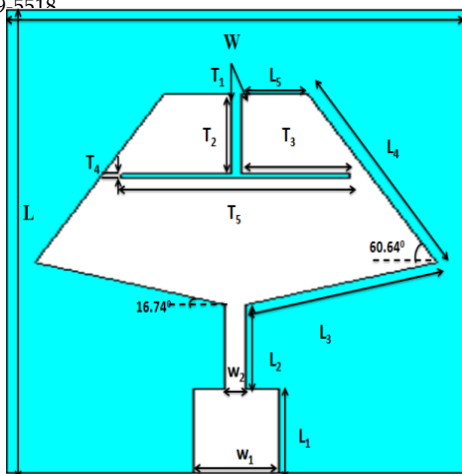
radiating patch [12]. A diamond shaped patch antenna is also used for achieving the multiband operation with the UWB range [13]. In [13] DSP antenna multiband operation is achieved by inserting a notched region in the middle part of the DSP antenna and adding quarter-wavelength strips. Multiband antenna with the reconfigurable facility is also the solution of the wide band width of the antenna. For the switching operations of these antennas PIN and varactor diodes are used. Now days MEMS switches are also used for this multiband operation [14],[15],[16].

2 PROPOSED ANTENNA DESIGN

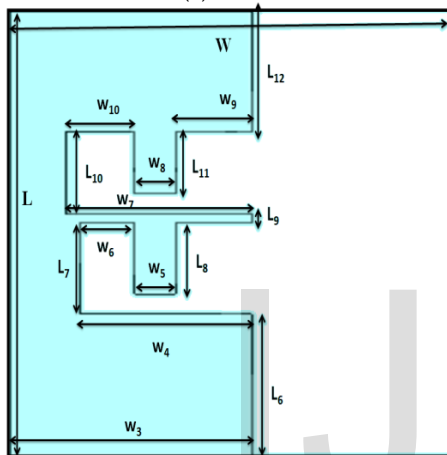
The proposed diamond shaped microstrip patch antenna is fed by the rectangular feeding line with the quarter wave transformer as shown in Fig.1. This proposed antenna is printed on the FR-4 substrate with the dimension of $22 \times 16 \text{ mm}^2$ and the thickness of 1 mm. The FR-4 substrate which is used for the designing of antenna has the relative permittivity of 4.05 with the loss tangent of 0.02.

The diamond shaped antenna has the inverted T-slot on the radiating patch and the E-slot in the partial ground of the antenna. The microstrip feeding line is fixed at the width $W_2 = 0.7 \text{ mm}$ and the length $L_2 = 4 \text{ mm}$. The length of the quarter wave length transformer has $L_1 = 4 \text{ mm}$ and the width $W_1 = 3 \text{ mm}$ is used for the impedance matching between the input port of the signal and the output port of the signal to the radiating patch of the antenna. The matching impedance of the proposed antenna structure is 60.67 ohm.

The diamond shape patch antenna with full ground is operate signal band of frequency when there is no inverted T-slot in the patch when we use the inverted T-slot in the radiating patch of the antenna than it operates as the dual band antenna thus this T-slot is responsible second band of the antenna. Now we change the dimension of this T-slot and also design



(a)



(b)

Fig. 1. (a) Proposed antenna design (top view), (b) Bottom.

TABLE 1
 DIMANSIONS OF PROPOSED ANTENNA DESIGN

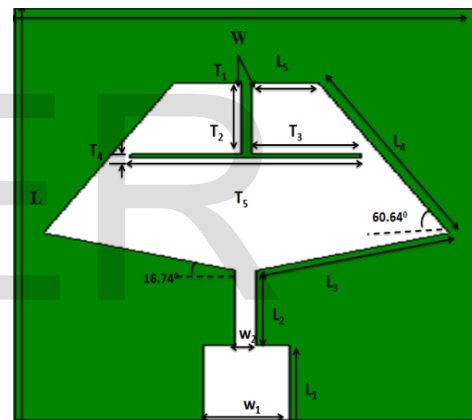
Antenna parameter	Value	Antenna parameter	Value
L	22mm	T ₃	3.8mm
L ₁	4mm	T ₄	0.2mm
L ₂	4mm	T ₅	8mm
L ₃	6.94mm	W	16mm
L ₄	9.178mm	W ₁	3mm
L ₅	2.3mm	W ₂	0.7mm
L ₆	7mm	W ₃	8.75mm
L ₇	4.5mm	W ₄	6.25mm
L ₈	3mm	W ₅	1.5mm
L ₉	0.5mm	W ₆	2mm
L ₁₀	3mm	W ₇	6.75mm
L ₁₁	6mm	W ₈	1.5mm
T ₁	0.4mm	W ₉	1.25mm
T ₂	3.8mm	W ₁₀	2.5mm

an E-slot in the radiating patch of the antenna than this antenna work at the triple frequency band. These bands are centered at the frequency 3.4069 GHz, 7.4132 GHz and the 10.678 GHz, these bands are useful for the communication application, the first band is cover the range of Wimax, second operates at C-band and third band is used for the fixed satellite service.

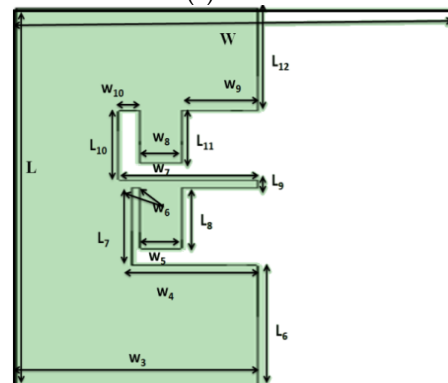
The dimension of this inverted T-slot is responsible for the second and the third band of the antenna, these bands of frequency can be changed by the changing the dimension of the T-slot T₂, T₃, T₄, T₅ and W. These bands also depends on the dimensions of the E-slot in the ground plan so they can also change by varying the parameter of the E-slot of the ground plan.

3 MODIFIED DESIGN OF PROPOSED ANTENNA

The modified structure of the proposed antenna is shown in the Fig.2. In this design the dimension of the E-slot of the ground plan is optimized and the T-slot of the radiating patch is fixed.



(a)



(b)

Fig. 2. (a) Modified antenna design (top view), (b) Bottom.

By changing the little dimension of the E-slot of the ground plan we increases the one frequency band of the proposed antenna and this modified structure workable up to four frequency band. This band is controlled by the dimension of the

E-slot in the ground plan. This modified antenna covers the four frequency bands which are centered at the resonant frequency 4.4322 GHz, 5.3943 GHz, 8.6262 GHz and the 11.262 GHz. These bands are useful for the communication application, the first band is cover the range of 4generation system (4.6-5.2 GHz), second operates for WLAN(5.15-5.823 GHz) , third band is use for the ITU band application and the fourth band is used for the fixed satellite services(10.567-11.43 GHz).

TABLE 2
 DIMANSIONS OF MODIFIED ANTENNA DESIGN

Antenna parameter	Value	Antenna parameter	Value
L_8	3.5mm	W_4	4.55mm
W_6	0.3mm	W_7	5.05mm
W_8	2.75mm	W_{10}	0.8mm

4 RESULT AND DISCUSSION

The proposed antenna is simulated by the help of the Electromagnetic (EM) simulation software. The microstrip patch antennas are simulated and optimized with the help of this software. The E-field and H-field radiation patterns, VSWR, return loss, surface current and Gain of both antennas are discussed in this section.

4.1 Case-I Simulated Results of Proposed Structure

The designed proposed antenna works for the triple band of frequency with the operating frequency range from 3.4069 GHz to 10.678 GHz. These three bands of frequency are centered at the 3.4069 GHz, 7.4132 GHz and 10.678 GHz and all bands are lies below than -10 dB so these bands are workable for the proposed antenna. The return loss of this antenna shows in the Fig.3.

From the Fig.3 it is very clear that this antenna is work at the resonant frequencies 3.4069 GHz, 7.4132 GHz and 10.678 GHz, which are useful for the Wimax, and fixed satellite service. The VSWR of this antenna is shown by the Fig.4 and this figure indicates that the impedance bandwidth of the proposed antenna.

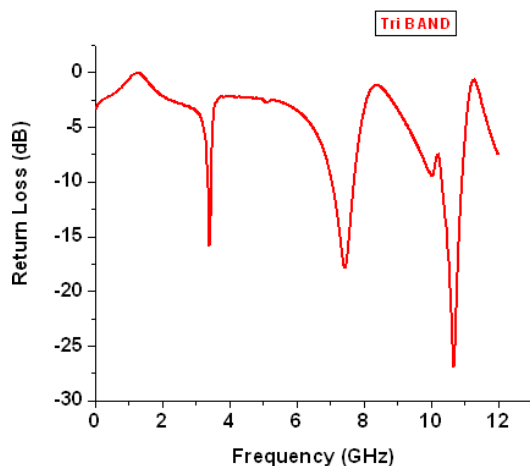


Fig. 3. Return loss of proposed antenna structure.

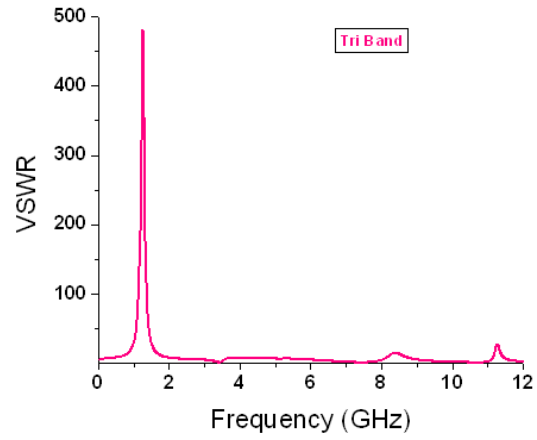


Fig. 4. VSWR of the proposed antenna structure.

The simulated radiation patterns of the proposed antenna are shown in the Fig.5, 6 and 7. The radiation pattern of the antenna is simulated for the E-plane and H-plane. These radiation patterns of the antenna are simulated for all the operating frequency of the antenna. From the Fig.5, 6 and 7 it is clear that the antenna is radiated in all direction because the radiation pattern of antenna is Omni directional in nature.

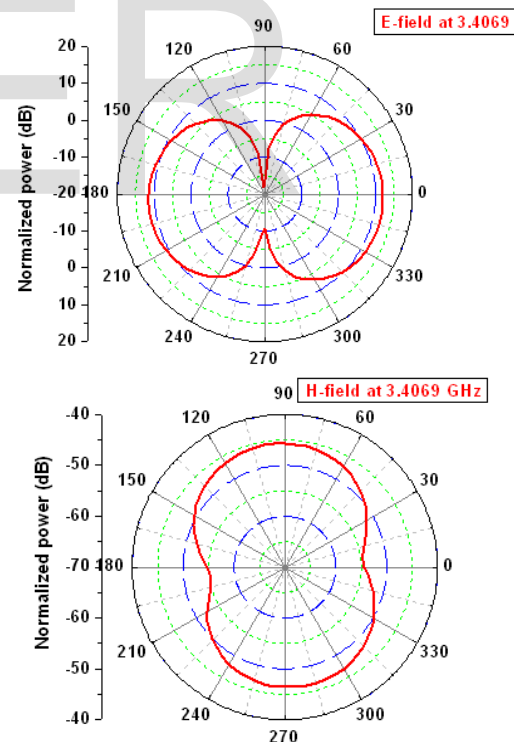


Fig. 5. Radiation pattern of proposed antenna structure at 3.4069 GHz.

The radiation pattern shown in Fig.5, 6 and 7 are shows the frequency band of 3.4069 GHz, 7.4132 GHz and 10.678 GHz respectively show the good agreement.

When the E-slot of the ground plan and inverted T-slot of the

antenna has any change than the radiation pattern of antenna can be change linearly. The E-plane radiation pattern of the antenna is working as y-z plane with the feeding line and normal to the substrate of the antenna while H-plane radiation pattern in x-z plane working normal to the feeding line.

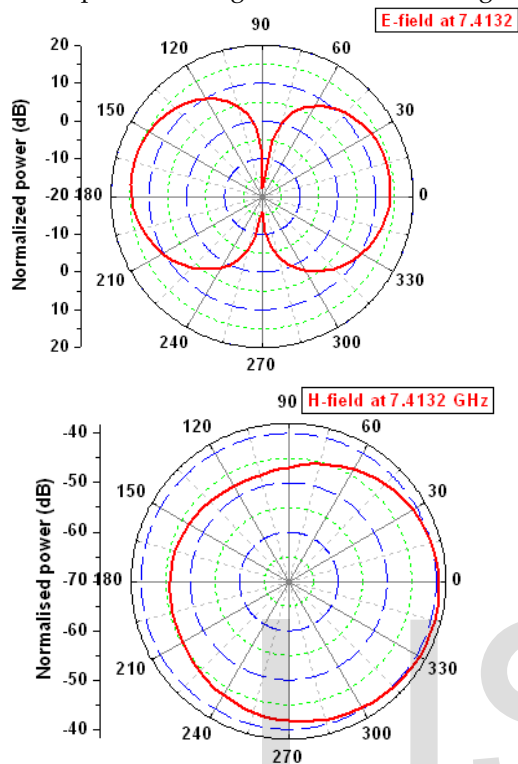


Fig. 6. Radiation pattern of proposed antenna structure at 7.4132 GHz.

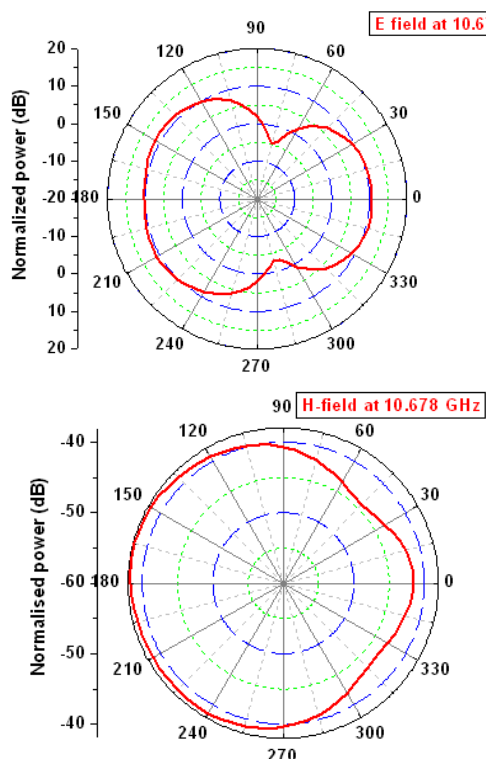


Fig. 7. Radiation pattern of proposed antenna structure at 10.678 GHz.

Fig. 8 shows the main parameter of the antenna, known as the antenna gain. The simulated gain of proposed antenna is covering the range of frequency from 0 to 12 GHz. The gain of antenna for the 0-12 GHz is achieved from -20 dBi to 8 dBi.

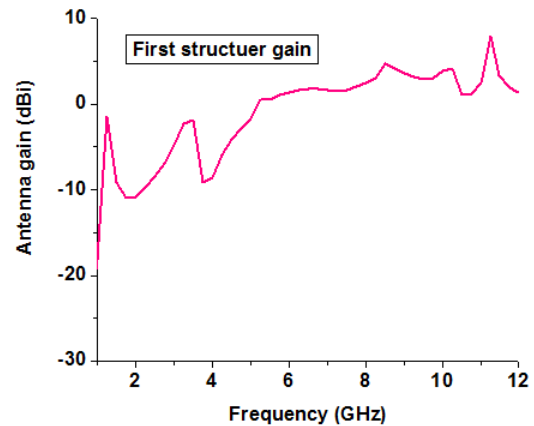


Fig. 8. Gain of proposed antenna structure.

The surface current of the antenna is also a useful and important parameter for the antenna. The Fig.9, 10 and 11 shows the surface current for the proposed antenna at the centered frequency at 3.4069 GHz, 7.4132 GHz and 10.678 GHz.

From the Fig.9 and 10 it is very clear that the mainly current flow in the antenna at the 3.4069 GHz and 7.4132 GHz is due to E-slot in the ground plan and this current flows from upward direction in the edges of the E-slot and downward towards the feeding line, at the edges of the E-slot the surface current is flows its maximum values while in the feeding line the surface current is reduce and there is very small current flows in the T-slot in the coming direction. At the center frequency 10.678 GHz, the current flow to the upward direction at its lowest value in the E-slot and the feeding line and these current flows up to its maximum value in the T-slot of the radiating patch in the outward direction.

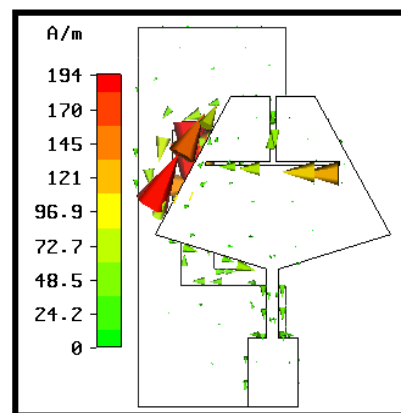


Fig. 9. Current distribution of proposed antenna structure at 3.4069 GHz.

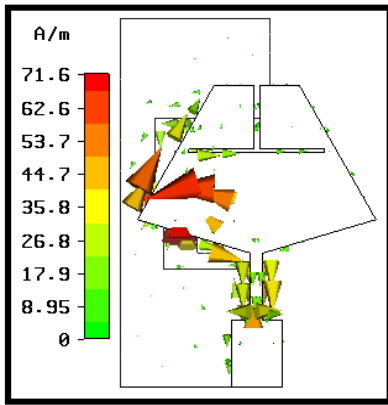


Fig10. Current distribution of proposed antenna structure at 7.4132 GHz.

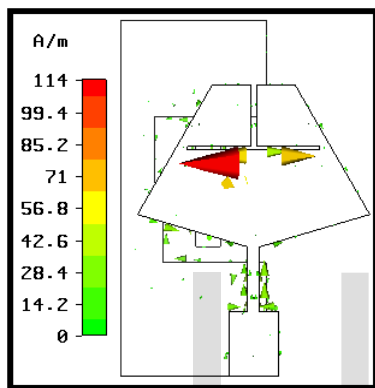


Fig. 11. Current distribution of proposed antenna structure at 10.678 GHz.

4.2 Case-II Simulated Results of Modified Structure

This modified antenna works for the four band of frequency with the operating frequency range from 4.432 GHz to 11.62 GHz. These four bands of frequency are centered at the 4.432 GHz, 5.39 GHz, 8.6278 GHz and 11.26 GHz and all bands are lies below than -10 dB so these bands are workable for the modified antenna. The return loss of this antenna shows in the Fig.12.

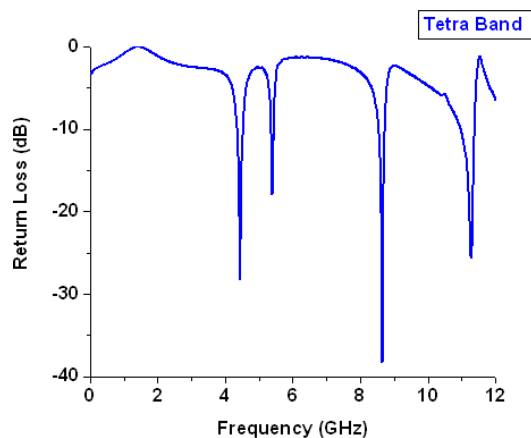


Fig. 12. Return loss of modified antenna structure.

From the Fig.12, it is very clear that this antenna is work at the resonant frequencies 4.432 GHz, 5.39 GHz and 8.6278 GHz and 11.26 GHz, which are useful for the 4G system, WLAN, ITU band application and the fixed satellite services. The VSWR of this antenna is shown by the Fig.13 and this figure also indicates that the impedance bandwidth of the proposed antenna.

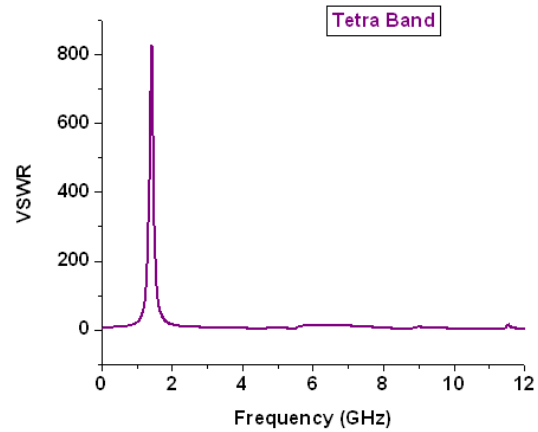


Fig. 13. VSWR of modified antenna structure.

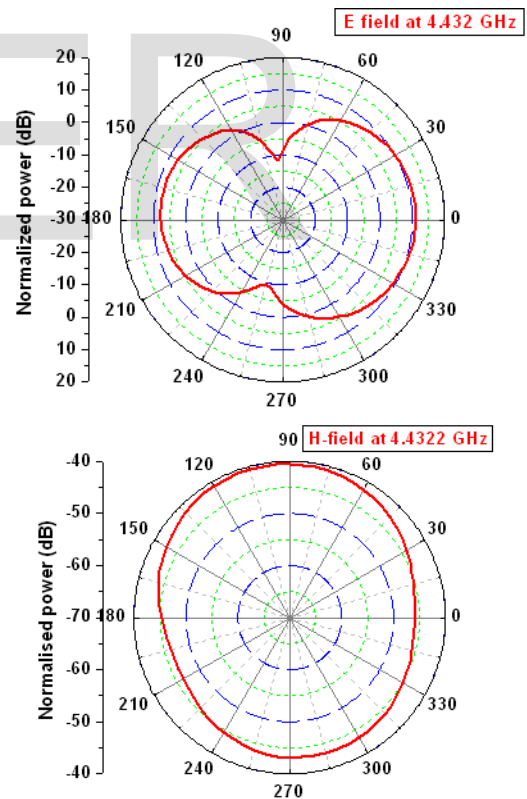


Fig. 14. Radiation pattern of modified antenna structure at 4.4322 GHz.

The simulated radiation patterns of the proposed antenna are shown in the Fig.14, 15, 16 and 17. The radiation pattern of the modified antenna is simulated for the E-plane and H-plane.

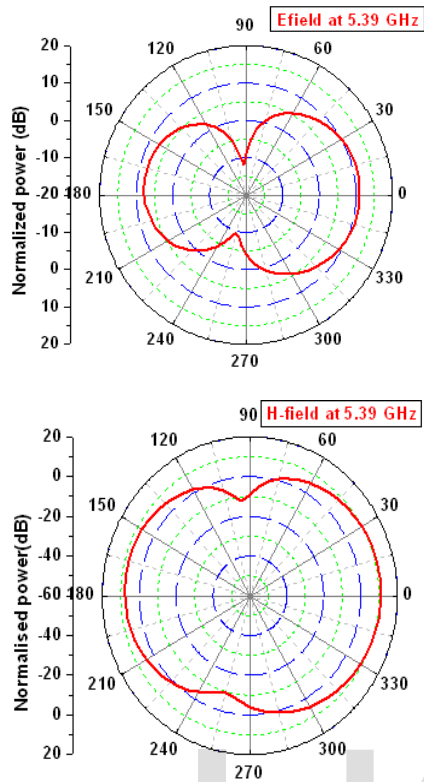


Fig. 15. Radiation pattern of Tetra-band antenna structure at 5.39 GHz.

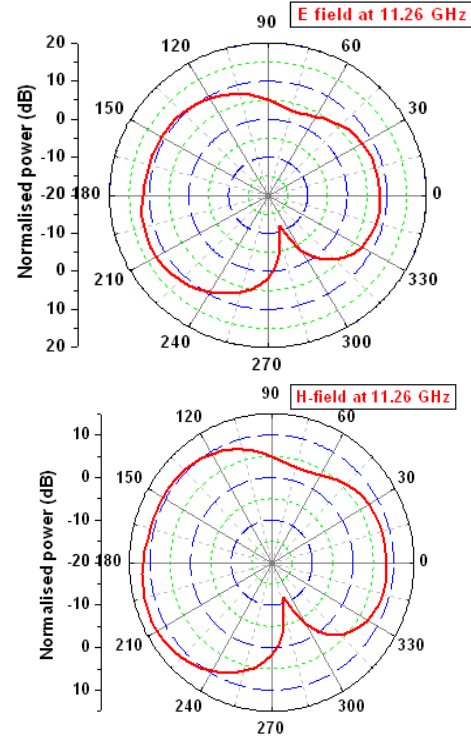


Fig. 17. Radiation pattern of Tetra-band antenna structure at 11.26 GHz.

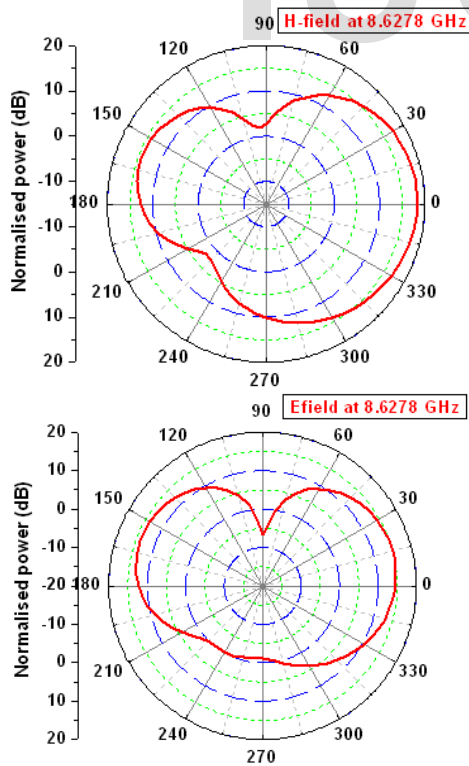


Fig. 16. Radiation pattern of modified antenna structure at 8.6278 GHz.

These radiation patterns of the antenna are simulated for all the operating frequency of the antenna. From the Fig.14, 15, 16 and 17 it is clear that the antenna is radiated in all direction because the radiation pattern of antenna is Omni directional in nature.

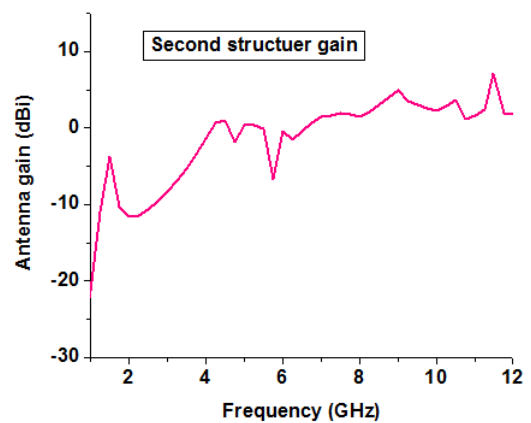


Fig. 18. Gain of modified antenna structure.

The radiation pattern shown in Fig.14, 15, 16 and 17 are shows the frequency band of 4.432 GHz, 5.39 GHz, 8.6278 GHz and 11.26 GHz respectively show the good agreement. When the E-slot of the ground plan and inverted T-slot of the antenna has any change than the radiation pattern of antenna can be

change linearly. The E-plane radiation pattern of the antenna is working as y-z plane with the feeding line and normal to the substrate of the antenna while H-plane radiation pattern in x-z plane working normal to the feeding line.

Fig. 18 shows gain parameter of the antenna. The simulated gain of proposed antenna is covering the range of frequency from 0 to 12 GHz. The gain of antenna for the 0-12 GHz is achieved from -20 dBi to 8 dBi.

The surface current of the antenna is also a useful and important parameter for the antenna. The Fig. 19, 20, 21 and 22 shows the surface current for the proposed antenna at the centered frequency at 4.432 GHz, 5.39 GHz, 8.6278 GHz and 11.26 GHz.

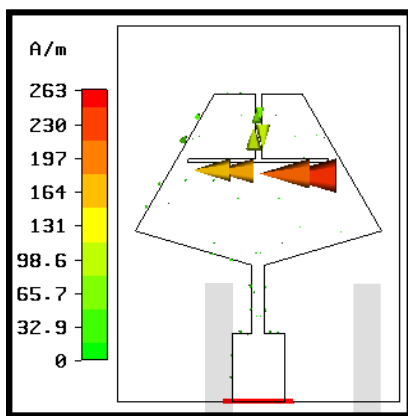


Fig. 19. Current distribution of proposed antenna structure at 4.4322 GHz.

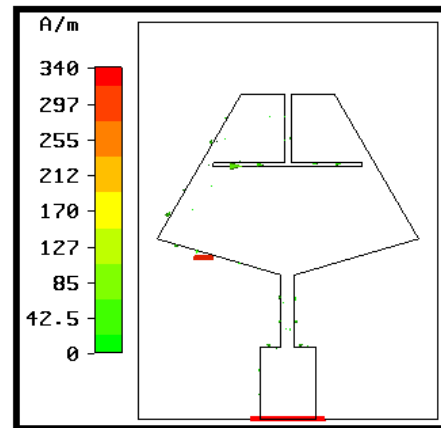


Fig. 21. Current distribution of proposed antenna structure at 4.4322 GHz.

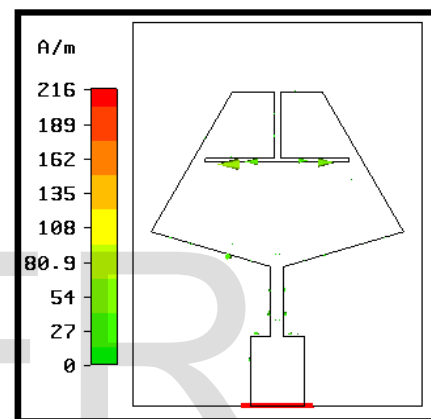


Fig. 22. Current distribution of proposed antenna structure at 8.6278 GHz.

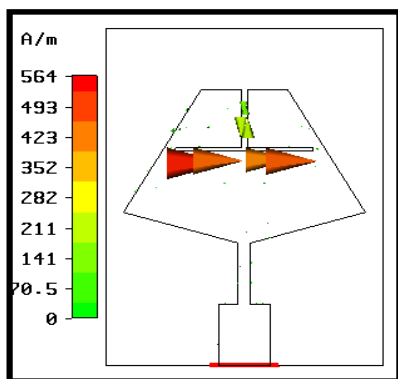


Fig. 20. Current distribution of proposed antenna structure at 5.39 GHz.

From the Fig.18 and 19 it is very clear that the mainly current flow in the antenna at the 4.432 GHz, 5.39 GHz and 11.26

GHz is due to inverted T-slot in the radiating patch and this current flows clockwise direction in 4.432 GHz, and anti-clockwise in 5.39 GHz, the current flowing at this frequency is very strong current and there is a very small current flowing in the edges of the E-slot in the ground plan. At the center frequency 8.6278 GHz and 11.26 GHz a very small current is flowing in the inverted T-slot and there is also a small current flowing in the E-slot of the ground plan.

4.3 Case-III Comparison of Case-I and Case-II

Fig. 23 shows the comparison of the simulated return losses of the proposed and modified structure of the antenna. From the above Figure it is clear that by the modified the E-slot of the ground plan the numbers of the frequency bands are increased.

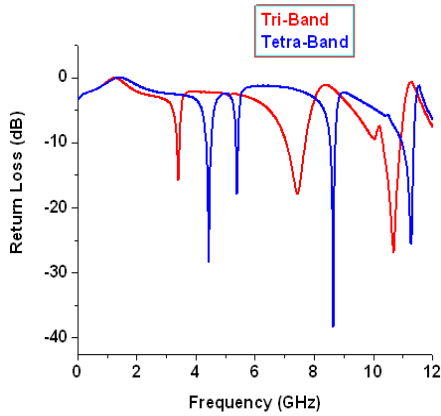


Fig. 23. Comparison of return losses of proposed and modified structure.

5 FABRICATED STRUCTURE AND RESULTS

Both antennas proposed and modified shown are fabricated on the FR-4 substrate. For designing of these structure FR-4 substrate of thickness $h = 1$ mm with Dielectric constant = 4.05 and loss tangent of the antenna is 0.02 is used.

For the measurement of the both antennas the vector network analyzer is used. The fabricated proposed and measured antenna structures are shown in Fig. 24.



(a)



(b)

Fig. 24. (a) Fabricated structure of the of proposed and modified structure (top view), (b) Bottom view

From the Fig.25, it is clear that the fabricated structure of the proposed antenna gives the approximately similar result to the simulated result of this antenna. First band of the simulated and fabricated structure is centered exact value of the center frequency 3.4069 GHz while the second and the third band of the antenna are shifted to their point of the center frequency. The second band shifted from to the 7.4132 GHz to 7.9547 GHz and third band is shifted from 10.678 GHz to 11.59 GHz.

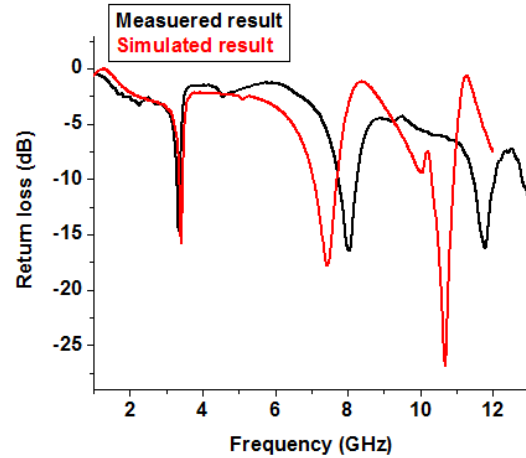


Fig. 25. Comparison of simulated and measured return losses of proposed antenna structure

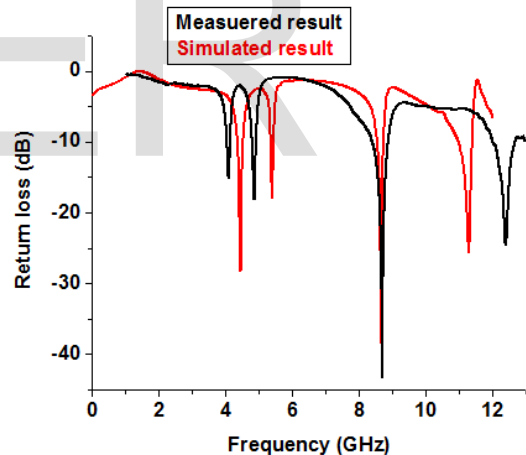


Fig. 26. Comparison of simulated and measured return losses of modified structure

The simulated return loss of the modified antenna structure is compared from the measured result of the fabricated modified structure is shown in Fig.26. From the Fig.26, it is clear that the fabricated structure of the proposed antenna gives the approximately similar result to the simulated result of this antenna. First and second band of the fabricated structure is centered at the 4.0197 GHz and second band 4.850 GHz while the third band occur exactly the same center frequency 8.6730 GHz and the last band of the frequency is shifted from 11.26 GHz to 11.9542 GHz.

6 CONCLUSION

In this paper, a new design of antenna for multiband operation has been discussed. By cutting the slot in the ground plane and the radiating element, triple band and four bands can be achieved. These bands can be achieved by the proper dimension of inverted T-slot and the E-slot. From the measured result it is clear that the proposed antenna is useful for the 3.4069 GHz to 11.59 GHz frequency range while modified structure of this antenna is useful for the 4.0197 GHz to 11.9542 GHz frequency range. These antennas have very compact size structure and good performance in the obtained frequency bands. For the future aspects these antennas are changed to reconfigurable antennas by the use of the switching element like PIN diode, varactor diode or RF-MEMS switch in the designed structures.

REFERENCES

- [1] S. Sekine, H. Shoki, and H. Morishita, "Antennas for wireless terminal," *IEICE Trans. Commun.*, vol. E86-B, no. 3, pp. 1005-1015, Mar. 2003.
- [2] Z. N. Chen, T. S. P. See, and X. Qing, "Small printed ultrawideband antenna with reduced ground plane effect," *IEEE Trans. Antennas Propag.* vol. 55, no. 2, pp. 383-388, Feb. 2007.
- [3] J. R. Verbiest and G. A. E. Vandenbosch, "A novel small-size printed tapered monopole antenna for UWBWBAN," *IEEE Antennas Wireless Propag. Lett.*, vol. 5, pp. 377-379, 2006.
- [4] S. Radiom, H. Aliakbarian, G. A. E. Vandenbosch, and G. G. E. Gielen, "An effective technique for symmetric planar monopole antenna miniaturization," *IEEE Trans. Antennas Propag.*, vol. 57, no. 10, pp. 2989-2996, Oct. 2009.
- [5] D. Valderas, R. Alvarez, J. Melendez, I. Gurutzeaga, J. Legarda, and J. I. Sancho, "UWB staircase-profile printed monopole design," *IEEE Antennas Wireless Propag. Lett.*, vol. 7, pp. 255-259, 2008.
- [6] M. Gopikrishna, D. D. Krishna, C. K. Anandan, P. Mohanan, and K. Vasudevan, "Design of a compact semi-elliptic monopole slot antenna for UWB systems," *IEEE Trans. Antennas Propag.*, vol. 57, no. 6, pp. 1834-1837, Jun. 2009.
- [7] A. M. Abbosh and M. E. Bialkowski, "Design of ultra wideband planar monopole antennas of circular and elliptical shape," *IEEE Trans. Antennas Propag.*, vol. 56, no. 1, pp. 17-23, Jan. 2008.
- [8] J. Jung, W. Choi, and J. Choi, "A small wideband microstrip-fed monopole antenna," *IEEE Microw. Wireless Compon. Lett.*, vol. 15, no. 10, pp. 703-705, Oct. 2005.
- [9] J. Jung, W. Choi, and J. Choi, "A compact broadband antenna with an L-shaped notch," *IEICE Trans. Commun.*, vol. E89-B, no. 6, pp. 1968-1971, Jun. 2006.
- [10] M. Ojaroudi, C. Ghobadi, and J. Nourinia, "Small square monopole PIN diode or RF-MEMS switch antenna with inverted T-shaped notch in the ground plane for UWB application," *IEEE Antennas Wireless Propag. Lett.*, vol. 8, pp. 728-731, 2009.
- [11] M. Rostamzadeh, S. Mohamadi, J. Nourinia, Ch. Ghobadi, and M. Ojaroudi, "Square monopole antenna for UWB applications with novel rod-shaped parasitic structures and novel V-shaped slots in the ground plane," *IEEE Antennas and Wireless Propagation Letters*, vol. 11, 2012, pp 446-449.
- [12] Ratnesh Kumari and Mithilesh Kumar "Design of multiband antennas for wireless communication", IEEE CSNT
- [13] Ali Foudazi, Hamid Reza Hassani, and Sajad Mohammad ali nezhad, "Small UWB Planar Monopole Antenna With Added GPS/GSM/WLAN Bands," *IEEE Transactions On Antennas And Propagation*, Vol. 60, No. 6, June 2012
- [14] A. Sheta and S. Mahmoud, "A widely tunable compact patch antenna," *IEEE Antennas Wireless Propag. Lett.*, vol. 7, pp. 40-42, 2008.
- [15] A. Mak, C. Rowell, R. Murch, and C. Mak, "Reconfigurable multiband antenna designs for wireless communication devices," *IEEE Trans. Antennas Propag.*, vol. 55, no. 7, pp. 1919-1928, Jul. 2007.
- [16] S. Yang, C. Zhang, H. Pan, A. Fathy, and V. Nair, "Frequency-reconfigurable antennas for multiradio wireless platforms," *IEEE Microw. Mag.*, vol. 10, no. 1, pp. 66-83, Feb. 2009.